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Estimation of zero-plane displacement height and aerodynamic roughness length on rice fields

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1 **Title**

2 Estimation of zero-plane displacement height and aerodynamic roughness length on rice fields

3

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16 **Abstract**

17 The estimation of aerodynamic roughness length (z_0) and zero-plane displacement height (d) is of primary importance
18 in the application of a number of models that simulate soil-vegetation-atmosphere interactions at different spatial scales.
19 Many efforts to directly measure z_0 and d in the case of various surfaces were conducted in the past from multi-level
20 measurements of wind speed over homogeneous surfaces, but results reported in the literature are still rare for some
21 canopies and can only be used as a rule of thumb.

22 In this work, values of d and z_0 along the whole agricultural season for two rice fields located in northern Italy and
23 characterized by different irrigation managements (continuous flooding and intermittent irrigation) were obtained from
24 single level turbulence measurements performed by an eddy covariance (EC) system installed on the levee between the
25 two fields. Throughout the growing season, d and z_0 appeared to be well correlated (R^2 greater than 90%) with the
26 vegetation height (h_v) and the mean value of the ratio between d and h_v was about 0.75 for both rice fields, while the
27 ratio between z_0 and h_v was about 0.06 and 0.05 respectively for the flooded and the intermittent irrigation treatments.
28 Moreover, d and z_0 did not show any clear dependence on wind speed or stability conditions of the atmosphere.

29

30 **Riassunto**

31 Stime accurate della lunghezza aerodinamica (z_0) e dell'altezza di dislocamento (d) sono estremamente importanti per
32 molti modelli che simulano gli scambi di massa ed energia nei sistemi suolo-vegetazione-atmosfera a differenti scale
33 spaziali. In passato sono stati fatti molti sforzi per misurare direttamente z_0 e d attraverso rilevamenti multilivello della
34 velocità del vento su superfici vegetate in modo omogeneo: i risultati presenti in letteratura sono tuttavia ancora scarsi
35 per molte tipologie di vegetazione e di conseguenza spesso si ricorre a regole pratiche che forniscono una stima
36 approssimata dei valori di z_0 e d .

37 In questo studio, i valori di z_0 e d per l'intera stagione agraria si sono ottenuti da misure di turbolenza effettuate ad un
38 solo livello tramite una stazione micrometeorologica *eddy covariance* installata sull'argine di separazione tra due
39 appezzamenti coltivati a riso nel Nord Italia, caratterizzati da differenti gestioni irrigue (sommersione continua e
40 irrigazione intermittente con riso aerobico). I risultati mostrano che durante l'intera stagione agraria, z_0 e d sembrano

41 essere ben correlati (R^2 maggiore del 90%) con l'altezza della vegetazione (h_v): il valore medio del rapporto tra d e h_v è
42 pari a circa 0.75 per entrambi i trattamenti irrigui, mentre il rapporto tra z_0 e h_v è di circa 0.06 per il riso caratterizzato da
43 sommersione e 0.05 per il riso aerobico. Infine, nessuna chiara correlazione si è riscontrata tra le condizioni di stabilità
44 atmosferica o la velocità del vento ed i valori di z_0 e d .

45
46 **Keywords:** aerodynamic roughness length, zero-plane displacement height, eddy covariance, paddy field, aerobic rice,
47 northern Italy.

48
49 **Parole Chiave:** Lunghezza aerodinamica, altezza di dislocamento, tecnica eddy covariance, riso in sommersione
50 continua, riso aerobico, Nord Italia

51

52 **1 Introduction**

53 In many studies focusing on the estimation of flux exchanges in the soil-vegetation-atmosphere system at large scales
54 (meteorological modeling applications) or at the single field scale (micrometeorological data analysis), aerodynamic
55 roughness length and zero-plane displacement height are required (e.g., Sugita and Brutsaert 1990, Toda e Sugita 2003,
56 Zhou et al. 2006).

57 Generally, z_0 and d are estimated using the wind profile method, where three wind velocity measurements at different
58 heights above the ground have to be simultaneously performed (Stull 1988, Asanuma et al. 2000). This method is
59 particularly expensive and requires the use of a meteorological tower as a support for the anemometers installation
60 (Foken 2008). Moreover, the profile equation may not be applied where wind is very weak, and the vertical wind speed
61 gradient is smaller than the accuracy limit of the sensors (Gao et al. 2003). As a possible alternative to the approach
62 illustrated above, Rotach (1994) proposed the use of temperature and vertical wind velocity variances to estimate d and
63 successively z_0 through the resolution of the wind profile. This method is attractive, since it requires measurements at a
64 single level typically performed by eddy covariance stations. However, a rigorous application and validation of the
65 method over different areas has not been yet carried out, and thus its robustness is still not well understood (Toda and
66 Sugita 2003, Mori et al. 2010). Martano (2000) proposed a new approach to quantify z_0 and d by using a single-level
67 sonic anemometer data set. Starting from wind velocity, Reynolds stress and sensible heat flux dataset at one height, the
68 method for the determination of z_0 and d can be reduced to a simpler least square procedure for one variable only (Gao
69 et al. 2003). Values of z_0 and d can be determined from the similarity wind profile law from single-level measurements
70 of wind speed and sensible fluxes by solving a simple and straightforward one-dimensional minimum problem. The
71 procedure requires no specialized software and a very little computational effort, however, high frequency data (10 or
72 20 Hz) acquisition is recommended (Martano 2000). In a recent study of Graf et al. (2014) three different approaches
73 for estimating d and z_0 - including Martano's (2000) model - were investigated, showing the good correlation of the
74 Martano method with the results obtained by the other two more sophisticated models based on the flux-variance
75 similarity theory (Foken 2008).

76 Data for the on-site estimation of roughness length and displacement height are not always available, therefore, in many
77 soil-vegetation-atmosphere models (SVAT models), z_0 and d are approximated following simple rules of thumb. In
78 many land surface models, such as BATS (Biosphere- Atmosphere Transfer Scheme) and SiB (Simple Biosphere
79 model), z_0 and d are taken as constant in function of crop typology (Dorman and Sellers, 1989; Dickinson et al., 1993).
80 In the CLM (Common Land Model) (Dai et al., 2003), z_0 is taken as a constant ratio of vegetation height (i.e., $z_0 =$
81 $0.07h$). In other models, z_0 assumes values in the range 0.06-0.2 meters (Dudhia et al. 2005; Grell et al. 1995;
82 Hagemann 2002).

83 Only few researches tried to estimate roughness parameters on rice surfaces, and in many cases discrepancies in the
84 values of z_0 and d were reported (Kim et al. 2001). In the works of Gao et al. (2003), Kotani and Sugita (2005) and Tsai
85 and Tsuang (2005), z_0 for a rice paddy with a crop height of about 60 cm varied between 10^{-3} and 10^{-1} meters. From
86 these studies, it can be inferred that the z_0 value over rice paddies strongly varies with the site. Zeng and Wang (2007)
87 showed that z_0 over a cropland is not only dependent on the specific crops, but also on obstacles in the area such as
88 buildings, trees and the aboveground biomass. In addition to these factors, z_0 and d are strongly connected with the
89 evolution of the vegetation height, and their values change over the growing season (Jacob and Boxel 1988).
90 Nevertheless, in the literature the evaluation of the roughness parameters above rice fields during the entire growing

91 season is still absent. Crop homogeneity over the field, crop typology, stiffness of the stem are just some elements that
92 can influence roughness parameters (Hansen 1993, Jacob and Boxel 1988).
93 In this technical note d and z_0 were evaluated using the Martano's (2000) method over the entire growing season for a
94 traditional paddy rice field and an aerobic rice field in northern Italy, and the obtained results were compared with the
95 standard prediction methods quoted in the literature. The peculiarity of this study lies also in using only one EC system
96 to monitor these aerodynamic parameters for the two different fields. Moreover, this technical note gives a contribution
97 to the increasing of experimental information on rice crop in northern Italy, which are still scarce.

98

99 **2 Material and Methods**

100 **2.1 Experimental set-up and measurements**

101 In the agricultural season 2013 an intensive monitoring activity was carried out at the National Rice Research Centre
102 (NRRC) located in Castello d'Agogna (Pavia, Italy) (45°14'49.64''N, 8°41'55.32''E) over rice fields under different
103 water regimes (Fig. 1). A complete description of the site characteristics and the instrumentation installed is reported in
104 Facchi et al. (2013) and Masseroni et al. (2014). In this paper, only instruments necessary to measure the variables used
105 into the Martano's (2000) method are described.

106 A 3D sonic anemometer (Young RM-81000, Campbell Scientific, USA) was installed in early June 2013 on the narrow
107 levee separating two rice fields characterized by different irrigation treatments: intermittent irrigation (IRR) and
108 continuous flooding (FLD). This choice was done to verify the possibility of using only one eddy covariance system for
109 monitoring turbulence fluxes (latent heat, LE, and sensible heat, H) in two different rice environments, and also because
110 of the limited size (40m x 80m) of the experimental fields. The instrument was held at about one meter over the canopy
111 along the whole monitoring period (7 June – 2 October). This choice was supported by the results shown in Arriga
112 (2008), who demonstrated that the quality of the measurements could be extremely compromised if the distance
113 between EC system and the surface (soil or top of a homogeneous canopy) is less than 30-40 cm. The sonic anemometer
114 was mounted on the top of an adjustable pole thrust into the soil. During the whole experimental period, the position of
115 the EC station was into the equilibrium boundary layer, which is a necessary condition for its proper operation as shown
116 in the work of Kaimal and Finnigan (1994). High frequency (10 Hz) wind velocity components and sonic temperature
117 data were stored in a compact flash card inserted into the CR5000 data logger (Campbell Scientific, USA) at which the
118 sonic anemometer was connected.

119 In addition to the continuous monitoring, periodic measurement campaigns (12 dates) were carried out to monitor the
120 crop biometric parameters along the cropping season (crop height, leaf area index).

121

122 Fig. 1. Experimental fields and EC system position. The complete description of the site characteristics and monitoring
123 activity are illustrated in Facchi et al. (2013).

124 Fig. 1. Campi sperimentali e posizionamento della stazione eddy covariance. La descrizione completa delle
125 caratteristiche del sito e delle attività di monitoraggio sono riportate in Facchi et al. (2013).

126

127 **2.2 Analytical procedure**

128 For the application of the Martano's (2000) method the wind profile is approximated by Eq. 1:

129

130
$$\bar{u} = \frac{u^*}{k} \left[\ln \left(\frac{z_m - d}{z_0} \right) - \psi_m \left(\frac{z_m - d}{L} \right) \right] \quad (1)$$

131

132 where \bar{u} is the mean wind speed over the average time (30 minutes interval), u^* and L represent the friction velocity
 133 and the Obukhov length, z_m denotes the measurement height, while k is the von Karman constant equal to 0.4. ψ_m
 134 represents the integrated universal momentum function (Foken 2008), in which the small dependence on z_0/L can be
 135 neglected (Sozzi 2002).

136 The Obukov length is defined by Eq. 2:

137

138
$$L = - \frac{(u^*)^3 T_v \rho c_p}{kg H_v} \quad (2)$$

139

140 where T_v is the virtual temperature, g is the acceleration due to gravity (9.81 m s^{-2}), ρc_p is the volumetric heat
 141 capacity at a constant pressure (with $c_p = 1005 \text{ J kg}^{-1} \text{ K}^{-1}$), and H_v is the buoyancy flux (virtual heat). Here we
 142 approximate H_v and T_v by the heat flux and mean temperature based on the sonic temperature. Using variables based
 143 on the sonic temperature has the advantage that no additional humidity sensor (with possible failures) is needed (Graft
 144 et al. 2014)..

145 ψ_m is most commonly calculated by Eq. 3 for unstable conditions ($z_m/L < 0$) of the atmosphere (Paulson 1970):

146

147
$$\psi_m \left(\frac{z_m - d}{L} \right) = \ln \left[\frac{1 + x^2}{2} \left(\frac{1 + x}{2} \right)^2 \right] - 2 \arctan x + \frac{\pi}{2} \quad (3)$$

148

149 with x defined as in Eq. 4:

150

151
$$x = \left(1 - \gamma \frac{z_m - d}{L} \right) \quad (4)$$

152

153 where γ is a universal constant equal to 19.3 (Hogstrom 1988).

154 For moderately stable conditions ($0 < z_m/L < 1$) of the atmosphere, ψ_m is computed as in Eq. 5:

155

156
$$\psi_m \left(\frac{z_m - d}{L} \right) = -\beta \frac{z_m - d}{L} \quad (5)$$

157

158 where β is another universal constant equal to 6.

159 If d is known, z_0 can be estimated from a single dataset of \bar{u} , u^* and L obtained from a single-level eddy-covariance
 160 station inverting Eq. 1, as shown in Eq. 6. Averaging across multiple points in time can be used to yield more robust
 161 results (averaged z_0), and the standard deviation σ_{z_0} can be used to quantify the uncertainty of the estimate (Martano
 162 2000).

163

$$164 \quad z_0 = \frac{z_m - d}{\exp\left[\frac{\bar{u}k}{u^*} + \psi_m\left(\frac{z_m - d}{L}\right)\right]} \quad (6)$$

165

166 If d is unknown, Martano's (2000) method provides a mathematical algorithm that iteratively allows to obtain d from the
 167 minimization of the variance of a S variable.

168 Let N be the total number of measurements belonging to a generic sector around the station in each half hourly time
 169 step. Each high frequency measurement will be constituted by u_i, u_i^*, L_i variables, where the index i defines the i _th
 170 measurement over the total dataset of N values.

171 Let d be a first approximate value of the displacement height (not necessary the optimum value), then S and σ_S can be
 172 defined by Eq. (7) and (8) respectively.

173

$$174 \quad S = \frac{1}{N} \sum_{i=1}^N \left[\frac{u_i k}{u_i^*} + \psi_m\left(\frac{z_m - d}{L_i}\right) \right] \quad (7)$$

175

$$176 \quad \sigma_S^2 = \frac{1}{N} \sum_{i=1}^N \left\{ \left[\frac{u_i k}{u_i^*} + \psi_m\left(\frac{z_m - d}{L_i}\right) \right] - S \right\}^2 \quad (8)$$

177

178 For each choice of the d value, a σ_S^2 value can be computed. The value of d at which corresponds the minimum value
 179 of σ_S^2 represents the optimal displacement height. Knowing d and applying Eq. (6) allows the calculation of the
 180 roughness parameter z_0 . For a detailed dissertation about the mathematical steps, the reader is referred to the Martano's
 181 (2000) work.

182

183 2.3 Quality and footprint-based data filtering

184 Before determining z_0 and d , measurements were filtered to ensure the quality of data in terms of good turbulence and
 185 wind speed according to the Mauder and Foken (2004) suggestions. In Tab. 1 the selection criteria are briefly
 186 summarized.

187

188 Tab. 1. Overview of the selection criteria for the application of the Martano's (2000) method

189 Tabella 1. Criteri di selezione dei dati per l'applicazione del metodo di Martano (2000).

190

191 To prevent situations dominated by an high fetch with fluxes predominantly coming from other fields in the
192 surrounding area, a detailed footprint analysis was performed on the acquired data. The Hisieh et al. (2000) analytical
193 model was applied with d and z_0 values of first approximation equal to $2/3h_v$ and $0.1h_v$ respectively (Foken 2008). A
194 circle with a radius equal to the distance between EC station and field edges (40 m in all the directions) was afterwards
195 considered: all half-hourly data corresponding to a modelled fetch that fell outside the circle were discarded. The fetch
196 calculated using the footprint model, was computed for a ratio between scalar flux and source strength (F/S_o) equals to
197 80%, according to Hsieh et al. (2000).

198 In order to determine d and z_0 estimates as a function of time during the growing season, Martano's (2000) method was
199 applied with a running window which advanced one day at time. Data were subdivided in two macro-groups as a
200 function of the wind direction. The first group gathered data coming from the northern sector (Sector I), while the
201 second group data coming from the southern sector (Sector II). In particular, data were taken into account only if the
202 wind direction was included in a range of 40° with respect to the North-South reference direction, as shown in Fig. 1.
203 Thus, unlike other works where data were divided into various sectors (Mori et al. 2010; Tsai et al. 2010), in this study
204 the number of sectors was reduced to one for each irrigation treatment (representing in total 80° over 360°).

205

206 **3 Results and discussion**

207 **3.1 Crop parameters**

208 Fig. 2 shows the height of the rice crops for the irrigation treatments FLD and IRR along the agricultural season 2013.
209 Dots represent the vegetation height measurements (h_v). A quadratic polynomial curve was used to interpolate the
210 experimental measurements, obtaining a good agreement in both the situations. Eddy covariance instruments height (z_m)
211 is also shown in the figure. Crop height was found to increase rapidly until about the middle of August when, more or
212 less at flowering, it reached the maximum value for both treatments. As showed in the figure, crop height in the IRR
213 field was lower than in the FDL field, with an average difference over the whole experimental period of about 12 cm.

214

215 Fig. 2. Crop height for rice in the FLD (on the left) and IRR (on the right) treatments: together with the measured data,
216 also an interpolating quadratic polynomial curve and the position of the eddy covariance instruments over the canopy
217 are reported.

218 Fig. 2. Altezza della coltura nei trattamenti irrigui FLD (a sinistra) e IRR (a destra): accanto ai dati misurati vengono
219 illustrate anche una curva interpolante polinomiale quadratica e la posizione della stazione eddy covariance al di sopra
220 della vegetazione.

221

222 **3.2 Displacement height and roughness length**

223 In Fig. 3 (a and b) the temporal patterns along the whole growing season of crop height (h_v), displacement height (d),
224 and roughness length (z_0) for the two rice crops are plotted. It can be noted that z_0 increases in the first part of the
225 growing season reaching a constant value of about 0.08 and 0.06 m between the end of July and the middle of August,
226 respectively for FDL and IRR. The d trend is similar to that of h_v : it increases rapidly in the first part of the growing
227 season, going from bare soil to a condition in which crop elements form a closed canopy, while from the end of August
228 it tends to decrease as a consequence of leaf senescence.

229 In Fig. 3 (c and d) the relationships between z_0 and d with respect to h_v are shown. The regression lines for the whole
230 experimental period were calculated with null intercept. For both treatments, the ratio d/h_v is about 0.75, while the ratio
231 z_0/h_v is about 0.06 and 0.05 for FDL and IRR respectively. In both cases, correlation coefficients are greater than 90%.
232 The regression coefficients found for FDL and IRR irrigation treatments are similar to each other, and in line with the
233 results reported in the literature for different crop typologies and different geographical regions (Tab.2).
234 As an additional analysis, the z_0 and d dependence from wind speed and stability condition of the atmosphere was
235 explored according to the methodology described in Hansen (1993) and Gao et al. (2003). Hansen (1993) showed that d
236 and z_0 could also be a function of wind speed. In fact, when the wind speed increases, the canopy tends to flex in the
237 along wind direction and flattening reduces the crop height (Foken 2008). Moreover, Motheith (1965) attributed the
238 variations of d and z_0 values to a transfer of momentum from the canopy top to layers deeper in the canopy and this
239 phenomenon is strongly correlated to the stability conditions of the atmosphere. In our work, the correlation coefficient
240 was computed between geometrical parameters (d and z_0) and turbulent ones (wind speed and z_m/L) as suggested by
241 Hansen (1993). Despite the effort, no evident correlation between stability of the atmosphere or wind speed and
242 roughness parameters was found, given that correlation coefficients for both the irrigation treatments were less than 0.1.
243

244 Fig. 3. Changes in crop height (h_v), displacement height (d), and roughness length (z_0), during the whole growing season
245 for the IRR and FDL irrigation treatments (a and b), and regression analysis between d or z_0 and h_v for the two
246 treatments (c and d).

247 Fig. 3. Andamento dell'altezza culturale (h_c), dell'altezza di dislocamento (d) e della lunghezza di rugosità (z_0) durante
248 la stagione irrigua per i trattamenti IRR e FDL (a e b) e analisi di regressione tra d , z_0 e h_c per i due trattamenti (c e d).
249

250 Tab. 2. Comparison of z_0 and d relations with h_v observed in this study with those in other works.

251 Tab. 2. Confronto tra le relazioni tra z_0 , d e h_v osservate in questo studio con quelle proposte da altre ricerche.
252

253 4 Conclusion

254 The results achieved in this study show that the dependence of d and z_0 on h_v is very strong for rice crops in northern
255 Italy, whatever the irrigation management adopted (FDL or IRR). The regression coefficients between d or z_0 and h_v
256 proved to be very similar for the two irrigation treatments, and in line with the results reported in the literature for many
257 crop typologies around the world. For both the irrigation treatments, the ratio d/h_v was found to be about 0.75, while the
258 ratio z_0/h_v was calculated as about 0.06 and 0.05 respectively for FDL and IRR; correlation coefficients (R^2) were
259 always higher than 90%.

260 Martano's (2000) model proved to be a valid method to estimate the evolution of the aerodynamic roughness
261 parameters along the entire growing season. It demonstrates to be sensible to the different crop growing phases,
262 including senescence, when crop height tends to decrease.

263 If the in-situ estimation of roughness parameters using more complex profile methods is not feasible, the Martano's
264 method could be considered as a more viable alternative. General rules for estimating roughness parameters should be
265 taken into account only in cases where the direct measurement is impossible, and be based on crops and soil/climatic
266 conditions as close as possible to those in which the study is being conducted.
267

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273

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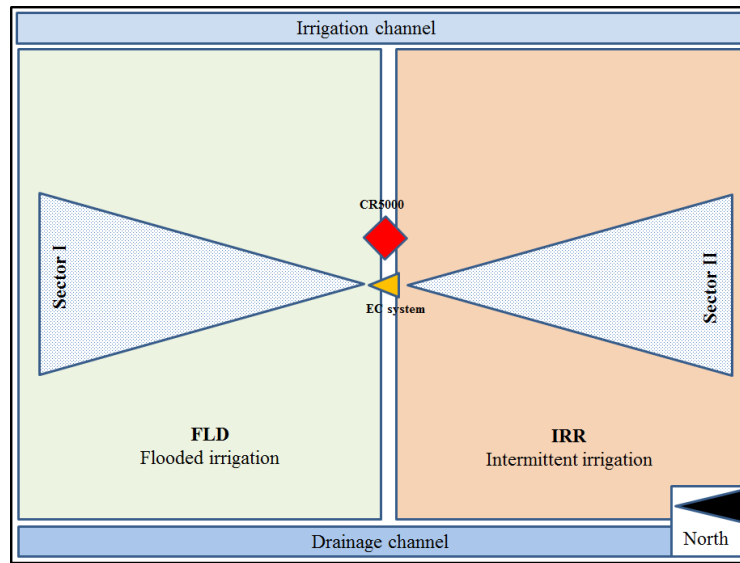
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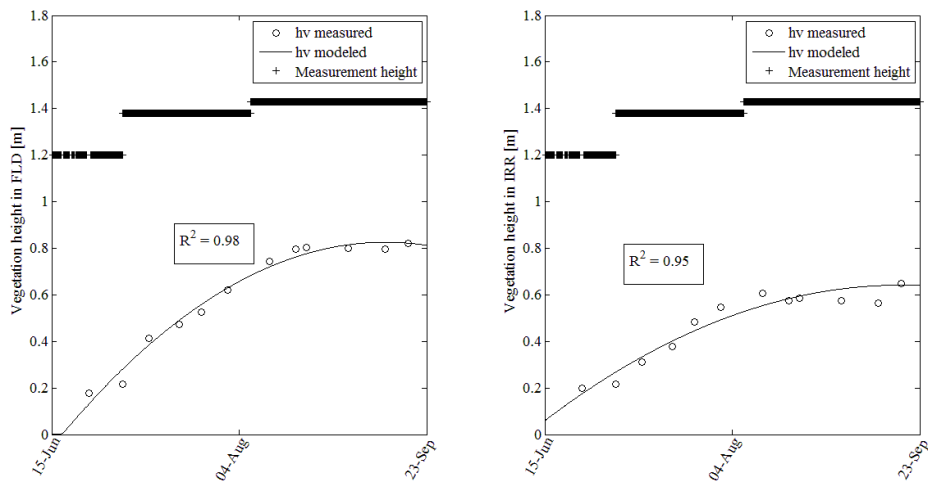
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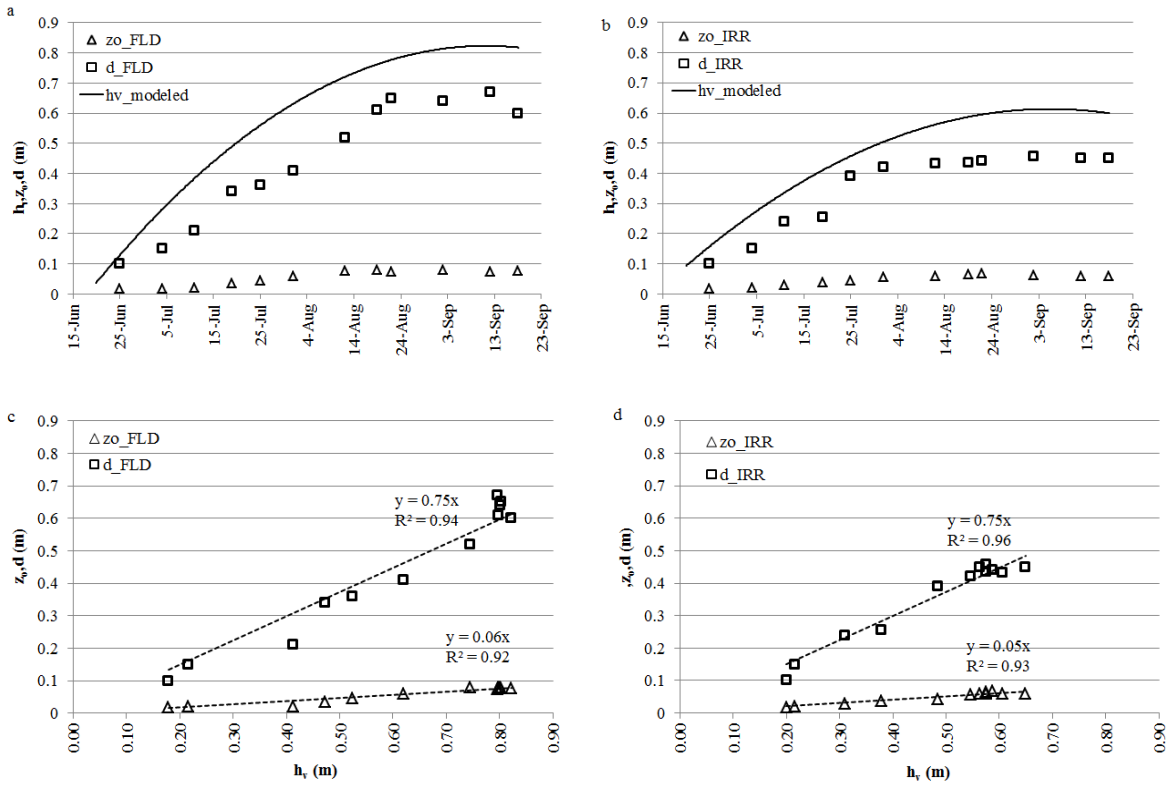
375 Fig. 1. Experimental fields and EC system position. The complete description of the site characteristics and monitoring
376 activity are illustrated in Facchi et al. (2013).
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379 Fig. 2. Crop height for rice in the FLD (on the left) and IRR (on the right) treatments: together with the measured data,
380 also an interpolating quadratic polynomial curve and the position of eddy covariance instruments over the canopy are
381 reported
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Fig. 3. Changes in crop height (h_v), displacement height (d), and roughness length (z_0), during the whole growing season for the IRR and FLD irrigation treatments (a and b), and regression analysis between d or z_0 and h_v for the two treatments (c and d)

390 **List of tables**

391 Tab. 1. Overview of the selection criteria for the application of the Martano (2000) method

Method	Variable	Selection criteria	Reference
Martano (2000)	u_i	$\bar{u} - 4\sigma_u < u_i < \bar{u} + 4\sigma_u$	Gao et al. (2003)
	\bar{u}	$\bar{u} > 1.5 [ms^{-1}]$	Graf et al. (2014)
	z_m/L	$-2 < \frac{z_m}{L} < 2$	Sozzi et al. (1997)

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394 Tab. 2. Comparison of z_o and d relations with h_v observed in this study with those in other works.

Author	z_o	d	Cultivation typology	Note
Nikaradze (1933) quoted in the work of Hansen (1993)	0.08 to 0.15 h_v	-	In crop not specified	-
Tanner and Pelton (1960) quoted in the work of Hansen (1993)	$\log z_o = a + b \log h_v$	-	Evaluated over different crops	Tanner and Pelton (1960) a = -0.883 b = 0.997 Sellers (1965) a = -1.385 b = 1.417 Kung (1963) a = -1.24 b = 1.19
Stanhill (1969) quoted in the work of Hansen (1993)	-	$\log d = 0.973 \log h_v - 0.1536$	Evaluated over different crops	-
Monteith (1965) quoted in the work of Hansen (1993)	-	$0.63h_v$	Evaluated over different crops	-
Thom (1972) quoted in the work of Jacob and Boxel (1988)	$z_o = k (h_v - d)$	-	Evaluated over different crops	Monteith (1973) for generic crops $k = 0.41$ Thom (1972) for a wheat crop

				$k = 0.37$ Seiger (1974) for a dense crop $k = 0.28$ Moore (1974) for generic crops $k = 0.26 \pm 0.07$ Shaw and Pereira (1982) obtained by their crop model $k = 0.29$
Jacob and Boxel (1988)	$z_0 = k (h_v - d)$	$0.75h_v$	Maize crop	$k = 0.25$
Foken (2008)	$0.1h_v$	$2/3 h_v$	Evaluated over different crops	-
Graf et al. (2014)	$z_0 = 0.06h_v + 0.02$	$d = 0.82h_v + 0.17$	Wheat crop	-
Gao et al. (2005)	-	$3/4 h_v$	Rice paddy	
This study	$0.06-0.05h_v$	$0.75h_v$	Rice (paddy and aerobic)	-

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